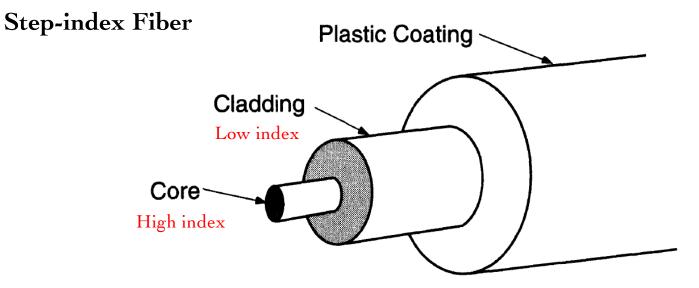
Chapter 5 Step-Index Circular Waveguide

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## Introduction of Circular Waveguides

• Widely used due to low cost



**Figure 5.1** The cylindrical step waveguide consists of a high-index core surrounded by a lower-index cladding.

#### Wave Equations in Cylindrical Coordinates

$$\mathbf{E}(r, \phi, z) = \hat{r}E_r(r, \phi, z) + \hat{\phi}E_{\phi}(r, \phi, z) + \hat{z}E_{z}(r, \phi, z)$$

Wave equation for planar waveguide  $\nabla^{2}\mathbf{E} - \mu\epsilon \frac{\partial^{2}\mathbf{E}}{\partial t^{2}} = 0$   $\nabla(\nabla \cdot \mathbf{E}) - \nabla \times \nabla \times \mathbf{E} - \mu\epsilon \frac{\partial^{2}\mathbf{E}}{\partial t^{2}} = 0$   $\frac{E_{z}}{r} \frac{E_{z}}{\partial r} \left(r \frac{\partial E_{z}}{\partial r}\right) + \frac{1}{r^{2}} \frac{\partial^{2}E_{z}}{\partial \phi^{2}} + \frac{\partial^{2}E_{z}}{\partial z^{2}} + k_{0}^{2}n^{2}E_{z} = 0$ 

**Figure 5.3** The longitudinal component of the electric field does not change through either propagation or reflection at the cylindrical surface.

Solution of Ez 
$$\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial E_z}{\partial r}\right) + \frac{1}{r^2}\frac{\partial^2 E_z}{\partial \phi^2} + \frac{\partial^2 E_z}{\partial z^2} + k_0^2 n^2 E_z = 0$$

- Separation of variables  $E_z(r, \phi, z) = R(r)\Phi(\phi)Z(z)$
- Substitute into the equation

$$R''\Phi Z + \frac{1}{r}R'\Phi Z + \frac{1}{r^2}R\Phi''Z + R\Phi Z'' + k_0^2n^2R\Phi Z = 0$$

- Multiple by  $r^2/R\Phi Z$  $r^2\frac{R''}{R} + r\frac{R'}{R} + \frac{\Phi''}{\Phi} + r^2\frac{Z''}{Z} + k_0^2n^2r^2 = 0$
- Assume a phase term for z dependence

 $Z(z) = e^{-j\beta z}$   $\beta: z$  component of the wavevector k in the waveguide.

$$r^{2}\frac{R''}{R} + r\frac{R'}{R} + \frac{\Phi''}{\Phi} - r^{2}\beta^{2} + k_{0}^{2}n^{2}r^{2} = 0 \longrightarrow r^{2}\frac{R''}{R} + r\frac{R'}{R} - r^{2}\beta^{2} + k_{0}^{2}n^{2}r^{2} = -\frac{\Phi''}{\Phi} = \nu^{2}$$

### Solution of Ez

$$r^{2}\frac{R''}{R} + r\frac{R'}{R} - r^{2}\beta^{2} + k_{0}^{2}n^{2}r^{2} = -\frac{\Phi''}{\Phi} = \nu^{2}$$

**T** "

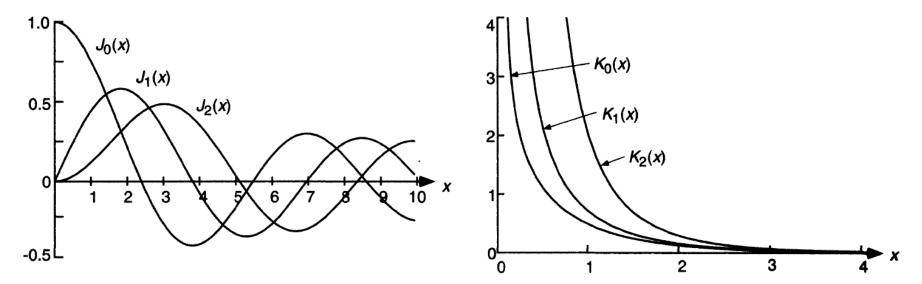
- Solve for  $\Phi$   $\nu$ : separation constant  $\Phi''(\phi) = -\nu^2 \Phi$   $\Phi(\phi) = Ae^{j\nu\phi} + c.c.$
- Substitute into  $r^2 \frac{R''}{R} + r \frac{R'}{R} + \frac{\Phi''}{\Phi} r^2 \beta^2 + k_0^2 n^2 r^2 = 0$

$$\longrightarrow r^2 \frac{\partial^2 R}{\partial r^2} + r \frac{\partial R}{\partial r} + r^2 \left( k_0^2 n^2 - \beta^2 - \frac{\nu^2}{r^2} \right) R = 0 \qquad \text{Only has} \\ R(r)$$

• Solve using Bessel functions

 $\begin{pmatrix} k_0^2 n^2 - \beta^2 - \frac{\nu^2}{r^2} \end{pmatrix} \begin{bmatrix} \text{positive Bessel functions of the first kind of order } \nu & J_{\nu}(\kappa r) \\ \kappa^2 = k_0^2 n^2 - \beta^2 \\ \text{negative modified Bessel functions of the second kind of order } \nu & K_{\nu}(\gamma r) \\ \gamma^2 = \beta^2 - k_0^2 n^2 \end{bmatrix}$ 

#### **Bessel Functions**



**Figure 5.4** Graphs show the first three Bessel functions of the first kind,  $J_{\nu}(\kappa r)$ , and of the second kind,  $K_{\nu}(\gamma r)$ .

$$J_{\nu}(\kappa r) \approx \sqrt{\frac{2}{\pi \kappa r}} \cos\left(\kappa r - \frac{\nu \pi}{2} - \frac{\pi}{4}\right)$$
 for  $\kappa r$  large

Damped sine wave Describe radial standing wave

$$K_{\nu}(\gamma r) \approx rac{e^{-\gamma r}}{\sqrt{2\pi\gamma r}}$$
 for  $hor$  large

Damped exponential wave Describe evanescent wave

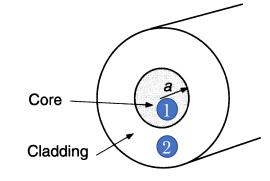
#### Field Distributions in the Step-Index Fiber

1. Oscillatory solution  $J_{\nu}(\kappa r)$   $\kappa^2 = k_0^2 n^2 - \beta^2$ 

$$\Rightarrow k_0 n_{core} > \beta > k_0 n_{clad}$$

2. Exponential decay  $K_{\nu}(\gamma r)$ 

for 
$$r < a$$
  $E_z(r, \phi, z) = AJ_\nu(\kappa r)e^{j\nu\phi}e^{-j\beta z} + c.c.$   
 $H_z(r, \phi, z) = BJ_\nu(\kappa r)e^{j\nu\phi}e^{-j\beta z} + c.c.$ 



**Figure 5.5** The cylindrical waveguide has a core radius of dimension *a*.

Solve boundary conditions for A, B, C, D

for 
$$r > a$$
  $E_z(r, \phi, z) = CK_\nu(\gamma r)e^{j\nu\phi}e^{-j\beta z} + c.c.$   
 $H_z(r, \phi, z) = DK_\nu(\gamma r)e^{j\nu\phi}e^{-j\beta z} + c.c.$ 

### Field Distributions in the Step-Index Fiber

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} = -\mu \frac{\partial \mathbf{H}}{\partial t} = -\mu j \omega \mathbf{H}$$

$$E_{\phi} = \frac{-j}{\alpha^{2}} \left( \frac{\beta}{r} \frac{\partial E_{z}}{\partial \phi} - \omega \mu \frac{\partial H_{z}}{\partial r} \right)$$
$$E_{r} = \frac{-j}{\alpha^{2}} \left( \frac{\mu \omega}{r} \frac{\partial H_{z}}{\partial \phi} + \beta \frac{\partial E_{z}}{\partial r} \right)$$
$$H_{\phi} = \frac{-j}{\alpha^{2}} \left( \omega \epsilon \frac{\partial E_{z}}{\partial r} + \frac{\beta}{r} \frac{\partial H_{z}}{\partial \phi} \right)$$
$$H_{r} = \frac{-j}{\alpha^{2}} \left( \beta \frac{\partial H_{z}}{\partial r} - \frac{\omega \epsilon}{r} \frac{\partial E_{z}}{\partial \phi} \right)$$
$$\downarrow$$
$$k_{0}^{2} n^{2} - \beta^{2}$$

### Field Distributions in the Step-Index Fiber

Core

Cladding

$$E_{r} = \frac{-j\beta}{\kappa^{2}} \left[ A\kappa J_{\nu}'(\kappa r) + \frac{j\omega\mu\nu}{\beta r} B J_{\nu}(\kappa r) \right] e^{j\nu\phi} e^{-j\beta z} \qquad E_{r} = \frac{j\beta}{\gamma^{2}} \left[ C\gamma K_{\nu}'(\gamma r) + \frac{j\omega\mu\nu}{\beta r} D K_{\nu}(\gamma r) \right] e^{j\nu\phi} e^{-j\beta z}$$

$$E_{\phi} = \frac{-j\beta}{\kappa^{2}} \left[ \frac{j\nu}{r} A J_{\nu}(\kappa r) - \frac{\omega\mu}{\beta} B \kappa J_{\nu}'(\kappa r) \right] e^{j\nu\phi} e^{-j\beta z} \qquad E_{\phi} = \frac{j\beta}{\gamma^{2}} \left[ \frac{j\nu}{r} C K_{\nu}(\gamma r) - \frac{\omega\mu}{\beta} D \gamma K_{\nu}'(\gamma r) \right] e^{j\nu\phi} e^{-j\beta z}$$

$$H_{r} = \frac{-j\beta}{\kappa^{2}} \left[ B\kappa J_{\nu}'(\kappa r) - \frac{j\omega\epsilon_{core}\nu}{\beta r} A J_{\nu}(\kappa r) \right] e^{j\nu\phi} e^{-j\beta z} \qquad H_{r} = \frac{j\beta}{\gamma^{2}} \left[ D\gamma K_{\nu}'(\gamma r) - \frac{j\omega\epsilon_{clad}\nu}{\beta r} C K_{\nu}(\gamma r) \right] e^{j\nu\phi} e^{-j\beta z}$$

$$H_{\phi} = \frac{-j\beta}{\kappa^{2}} \left[ \frac{j\nu}{r} B J_{\nu}(\kappa r) + \frac{\omega\epsilon_{core}}{\beta} A \kappa J_{\nu}'(\kappa r) \right] e^{j\nu\phi} e^{-j\beta z} \qquad H_{\phi} = \frac{j\beta}{\gamma^{2}} \left[ \frac{j\nu}{r} D K_{\nu}(\gamma r) + \frac{\omega\epsilon_{clad}}{\beta} C \gamma K_{\nu}'(\gamma r) \right] e^{j\nu\phi} e^{-j\beta z}$$

## Boundary Conditions for the Step-Index Waveguide

$$\begin{array}{ll} & \text{Boundary condition: r=a} & E_z, E_\phi, H_z, \text{ and } H_\phi \quad \text{continuous} \\ & \begin{bmatrix} J_\nu(\kappa a) & 0 & -K_\nu(\gamma a) & 0 \\ 0 & J_\nu(\kappa a) & 0 & -K_\nu(\gamma a) \\ \frac{\beta\nu}{a\kappa^2}J_\nu(\kappa a) & j\frac{\omega\mu}{\kappa}J'_\nu(\kappa a) & \frac{\beta\nu}{a\gamma^2}K_\nu(\gamma a) & j\frac{\omega\mu}{\gamma}K'_\nu(\gamma a) \\ -j\frac{\omega\epsilon_{core}}{\kappa}J'_\nu(\kappa a) & \frac{\beta\nu}{a\kappa^2}J_\nu(\kappa a) & -j\frac{\omega\epsilon_{clad}}{\gamma}K'_\nu(\gamma a) & \frac{\beta\nu}{a\gamma^2}K_\nu(\gamma a) \end{bmatrix} \begin{bmatrix} A \\ B \\ C \\ D \end{bmatrix} = 0 \\ \\ \frac{\beta^2\nu^2}{a^2} \left[\frac{1}{\gamma^2} + \frac{1}{\kappa^2}\right]^2 = \left[\frac{J'_\nu(\kappa a)}{\kappa J_\nu(\kappa a)} + \frac{K'_\nu(\gamma a)}{\gamma K_\nu(\gamma a)}\right] \quad \text{characteristic equation} \\ \\ \left[\frac{k_0^2n_{core}^2J'_\nu(\kappa a)}{\kappa J_\nu(\kappa a)} + \frac{k_0^2n_{clad}^2K'_\nu(\gamma a)}{\gamma K_\nu(\gamma a)}\right] \end{array}$$

Solution of A, B, C, D  

$$AJ_{\nu}(\kappa a) = CK_{\nu}(\gamma a) \qquad \longrightarrow \qquad C = \frac{J_{\nu}(\kappa a)}{K_{\nu}(\gamma a)}A$$

$$D = \frac{J_{\nu}(\kappa a)}{K_{\nu}(\gamma a)}B$$

Continu

Continuous 
$$E_{\phi}$$
  $B = \frac{j\nu\beta}{\omega\mu a} \left[ \frac{1}{\kappa^2} + \frac{1}{\gamma^2} \right] \left[ \frac{J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right]^{-1} A$   
Continuous  $H_{\phi}$   $B = \frac{j\omega a}{\beta\nu} \left[ \frac{n_{core}^2}{\kappa} \frac{J_{\nu}'(\kappa a)}{J_{\nu}(\kappa a)} + \frac{n_{clad}^2}{\gamma} \frac{K_{\nu}'(\gamma a)}{K_{\nu}(\gamma a)} \right] \left[ \frac{1}{\kappa^2} + \frac{1}{\gamma^2} \right]^{-1} A$ 

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#### Transverse Electric and Transverse Magnetic Modes

characteristic equation  $\frac{\beta^2 \nu^2}{a^2} \left[ \frac{1}{\gamma^2} + \frac{1}{\kappa^2} \right]^2 = \left[ \frac{J'_{\nu}(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right] \left[ \frac{J'_{\nu}(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right]$ 

• v: angular dependence of the solution

when 
$$\nu = 0$$

$$\begin{bmatrix} J'_{\nu}(\kappa a) \\ \kappa J_{\nu}(\kappa a) + \frac{K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)} \end{bmatrix} \begin{bmatrix} \frac{k_0^2 n_{core}^2 J'_{\nu}(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{k_0^2 n_{clad}^2 K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)} \end{bmatrix} = 0$$

$$B = \frac{j\nu\beta}{\omega\mu a} \begin{bmatrix} \frac{1}{\kappa^2} + \frac{1}{\gamma^2} \end{bmatrix} \begin{bmatrix} J'_{\nu}(\kappa a) \\ \kappa J_{\nu}(\kappa a) + \frac{K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)} \end{bmatrix}^{-1} A \qquad B = \frac{j\omega a}{\beta\nu} \begin{bmatrix} \frac{n_{core}^2 J'_{\nu}(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{n_{clad}^2 K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)} \end{bmatrix} \begin{bmatrix} \frac{1}{\kappa^2} + \frac{1}{\gamma^2} \end{bmatrix}^{-1} A$$
Continuous  $E_{\phi}$ 

$$M = 0.$$

$$E_{z=0}$$

$$TE \text{ mode}$$

$$TM \text{ mode}$$

# Find propagation vector $\boldsymbol{\beta}$

Solve 
$$\left[\frac{J'_{\nu}(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)}\right] \left[\frac{k_0^2 n_{core}^2 J'_{\nu}(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{k_0^2 n_{clad}^2 K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)}\right] = 0$$

Simplified using Bessel relation

$$\frac{J_{\nu}'}{\kappa J_{\nu}} = \pm \frac{J_{\nu \mp 1}}{\kappa J_{\nu}} \mp \frac{\nu}{\kappa^2}$$

$$\frac{K'_{\nu}}{\gamma K_{\nu}} = \mp \frac{K_{\nu \pm 1}}{\gamma K_{\nu}} \mp \frac{\nu}{\gamma^2}$$

TE: 
$$\left[\frac{J'_{\nu}(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K'_{\nu}(\gamma a)}{\gamma K_{\nu}(\gamma a)}\right] = 0 \quad \longrightarrow \quad -\frac{J_{1}(\kappa a)}{\kappa J_{0}(\kappa a)} - \frac{K_{1}(\gamma a)}{\gamma K_{0}(\gamma a)} = 0$$

$$\text{TM:} \left[ \frac{k_0^2 n_{core}^2 J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{k_0^2 n_{clad}^2 K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right] = 0$$

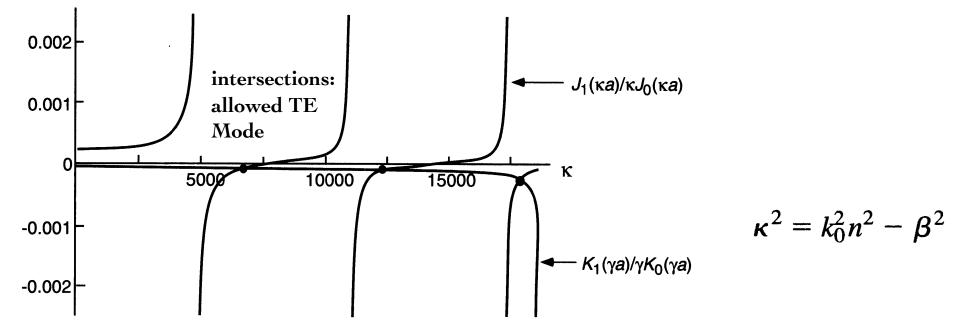
Need to solve numerically

## Example of TE Mode

$$-\frac{J_1(\kappa a)}{\kappa J_0(\kappa a)} - \frac{K_1(\gamma a)}{\gamma K_0(\gamma a)} = 0$$

determine the allowed eigenvalues for  $\beta$  for the TE modes.

core radius 
$$a = 5 \mu m$$



**Figure 5.6** The eigenvalue equation is plotted against  $\kappa$  for a waveguide with core index 1.5, cladding index 1.45, and wavelength  $1.3\mu$ m.

## Hybrid Mode

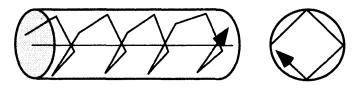
- $\nu \neq 0$ : both Ez and Hz
- if A = 0 then the mode is called a
- if B = 0 then the mode is called a
- if A > B then the mode is called an
- if A < B then the mode is called an

TE mode

TM mode

HE mode ( $E_z$  dominates  $H_z$ )

EH mode ( $H_z$  dominates  $E_z$ )



Skew Ray (EH or HE Mode)

**Figure 5.8** A skew ray travels in a spiral path down the fiber. The ray does not go through the origin.

## Linearly Polarized Mode

$$\frac{\beta^{2}\nu^{2}}{a^{2}} \left[ \frac{1}{\gamma^{2}} + \frac{1}{\kappa^{2}} \right]^{2} = \left[ \frac{J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right] \left[ \frac{k_{0}^{2}n_{core}^{2}J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{k_{0}^{2}n_{clad}^{2}K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right]$$
• weakly guiding approximation  

$$\Delta n = n_{core} - n_{clad} \text{ on the order of } 0.001-0.005 \qquad \qquad n_{core} \approx n_{clad} = n$$

$$\frac{\beta^{2}\nu^{2}}{a^{2}} \left[ \frac{1}{\gamma^{2}} + \frac{1}{\kappa^{2}} \right]^{2} = \left[ \frac{J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right]^{2} k_{0}^{2} n^{2} \qquad \text{if } n_{core} = n_{clad}, \text{ then } \beta^{2} = k_{0}^{2}n^{2}$$
using Bessel relation  $\frac{J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} = \pm \frac{J_{\nu \mp 1}}{\kappa a J_{\nu}(\kappa a)} \mp \frac{\nu}{\kappa^{2}a} \qquad \text{and} \qquad \frac{K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} = \frac{K_{\nu \pm 1}(\gamma a)}{\gamma a K_{\nu}(\gamma a)} \mp \frac{\gamma^{2}a}{\gamma^{2}a}$ 

$$\frac{J_{\nu \pm 1}(\kappa a)}{\kappa J_{\nu}(\kappa a)} = \mp \frac{K_{\nu \pm 1}(\gamma a)}{\gamma K_{\nu}(\gamma a)} \qquad \text{EH (top sign) and HE (bottom sign)}$$

$$\xrightarrow{\text{Bessel relation}} \qquad \kappa \frac{J_{j-1}(\kappa a)}{J_{j}(\kappa a)} = -\gamma \frac{K_{j-1}(\gamma a)}{K_{j}(\gamma a)}$$

#### Linearly Polarized Mode

$$\kappa \frac{J_{j-1}(\kappa a)}{J_j(\kappa a)} = -\gamma \frac{K_{j-1}(\gamma a)}{K_j(\gamma a)}$$

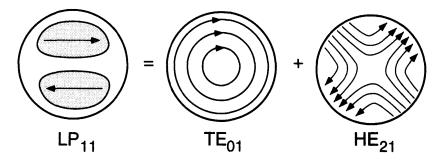
Degenerate modes

 $\begin{array}{ccc} TE_{0m} & \longleftrightarrow & TM_{0m} & & \text{Same } \beta \\ \\ HE_{\nu+1,m} & \longleftrightarrow & EH_{\nu-1,m} & & \text{Same } \beta \end{array} \end{array}$ 

define stable superpositions of different modeslinearly polarizedprimarily transverse

 $LP_{1m} \rightarrow \text{sum of } TE_{0m}, TM_{0m}, \text{ and } HE_{2m} \text{ modes}$   $LP_{\nu m} \rightarrow \text{sum of } HE_{\nu+1,m} \text{ and } EH_{\nu-1,m} \text{ modes}$  $LP_{0m} \rightarrow HE_{1m} \text{ mode only (special case)}$ 

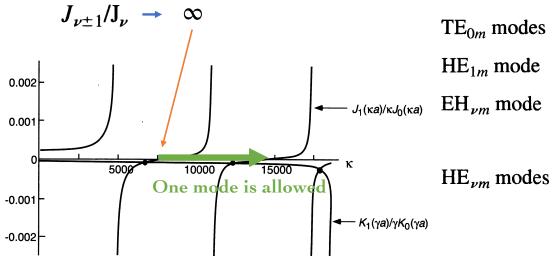
j = 1	TE, TM modes
$j = \nu + 1$	$\mathrm{EH}_{\nu}$ modes
$j = \nu - 1$	$HE_{\nu}$ modes



**Figure 5.9** The LP<sub>11</sub> mode is a superposition of the  $TE_{01}$  and  $HE_{21}$  modes. Note that the LP mode is linearly polarized, in contrast to the electric fields of the two constituent modes.  $E_x$  polarization is shown, although with appropriate superposition, an  $E_y$  polarized mode could have been created.

#### Normalized Frequency and Cutoff

$$\frac{\beta^2 \nu^2}{a^2} \left[ \frac{1}{\gamma^2} + \frac{1}{\kappa^2} \right]^2 = \left[ \frac{J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right] \left[ \frac{k_0^2 n_{core}^2 J_{\nu}'(\kappa a)}{\kappa J_{\nu}(\kappa a)} + \frac{k_0^2 n_{clad}^2 K_{\nu}'(\gamma a)}{\gamma K_{\nu}(\gamma a)} \right]$$

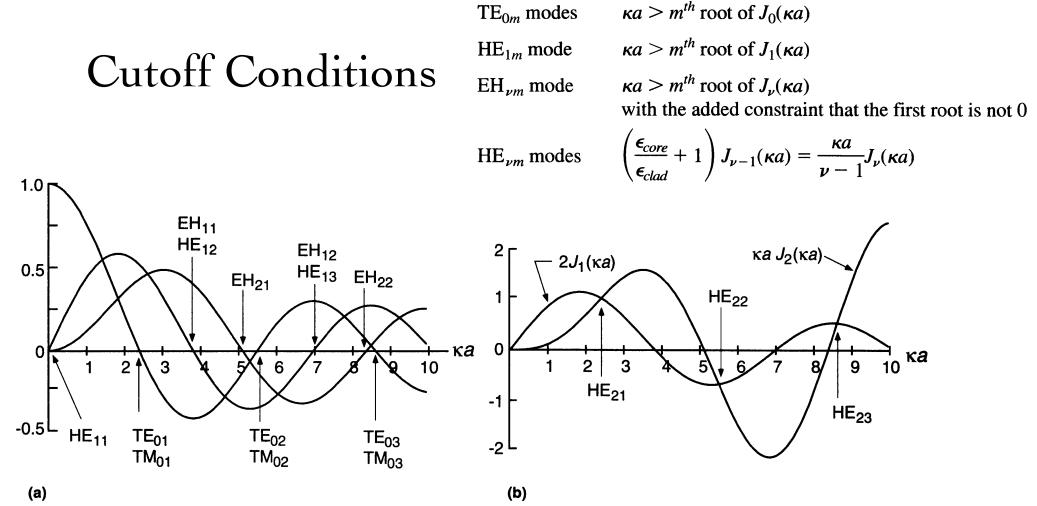


with the added constraint that the first root is not 0

$$\left(\frac{\epsilon_{core}}{\epsilon_{clad}}+1\right)J_{\nu-1}(\kappa a)=\frac{\kappa a}{\nu-1}J_{\nu}(\kappa a)$$

**Figure 5.6** The eigenvalue equation is plotted against  $\kappa$  for a waveguide with core index 1.5, cladding index 1.45, and wavelength 1.3 $\mu$ m.

core radius  $a = 5\mu m$ 



**Figure 5.11** The first three  $J_{\nu}$  Bessel functions are plotted, with the mode cutoff conditions of a few modes indicated at the various roots of the curves. The condition  $2J_1(\kappa a) = \kappa a J_2(\kappa a)$  is plotted for the HE<sub>2m</sub> mode cutoff conditions. Cutoff occurs where the curves cross.

### Normalized frequency (V number)

• V number:  $\kappa_{max}a$ V number =  $ak_0\sqrt{n_{core}^2 - n_{clad}^2} = \frac{2\pi a}{\lambda}\sqrt{n_{core}^2 - n_{clad}^2}$ 

• Example:

Consider a step-index fiber that has a core index  $n_{core} = 1.45$ , a cladding index  $n_{clad} = 1.44$ , and a core radius of  $25 \mu m$ . If the excitation wavelength is  $1.5 \mu m$ , how many TE and TM modes will exist in the waveguide?

$$V = \frac{2\pi 25\mu m}{1.5\mu m} \sqrt{1.45^2 - 1.44^2}$$
  
= 17.802

The zeros of the  $J_0(\kappa a) = 0$  occur at 2.405, 5.520, 8.654, 11.791, 14.931, 18.071

5 modes are allowed